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RESEARCH ARTICLE

COMPUTATIONAL THERMAL DESIGN OF FORCED DRAFT COUNTER TO CROSS FLOW AIR COOLED HEAT EXCHANGER AT NORMAL AMBIENT TEMPERATURE I.E. AT 38°C

*,1Parag Mishra and ²Dr Manoj Arya

¹Department of Mechanical Engineering, PhD Scholar, AISECT University Bhopal, MP India ²Department of Mechanical Engineering, MANIT Bhopal, MP, India

ARTICLE INFO

ABSTRACT

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Key words:

Thermal Design, Counter to cross flow heat exchanger, Thermal design problems, Uncertainties in design. Normal ambient temperature, Permissible/minimum tube Skin temperature. Heat exchangers are equipment that transfers heat from one medium to another. An air cooled heat exchanger, or ACHE, is simply a pressure vessel which cools a circulating fluid within finned tubes by forcing ambient air over the exterior of the tubes. In cross flow exchangers, the hot and cold fluids move perpendicular to each other. Some actual heat exchangers are a mixture of cross flow and counter flow (Known as Counter to Cross Flow Heat Exchangers) due to design features (Parag Mishra and Dr Manoj Arya, 2016). The proper design, operation and maintenance of heat exchangers will make the process energy efficient and minimize energy losses. Heat exchanger performance can deteriorate with time, off design operations and other interferences such as fouling, scaling etc. It is necessary to assess periodically the heat exchanger performance in order to maintain them at a high efficiency level. This section comprises certain proven techniques of monitoring the performance of heat exchangers, coolers and condensers from observed operating data of the equipment. In this we are doing the thermal design of forced draft counters to cross flow Air Cooled heat exchanger at normal ambient temperature i.e at 38 °C. The most important parameter, while taking into consideration of designing Air Cooled Heat Exchanger is permissible /minimum tube skin temperature. A major problem constantly faced by heat exchanger designers is to predict accurately the performance of a given heat exchanger or a system of heat exchangers for a given set of service conditions. The problem is complicated by the fact that uncertainties exist in most of the design parameters and in the design procedures themselves. The design parameters that are used in the basic thermal design calculations of a heat exchanger include process parameters, heat-transfer coefficients, tube dimensions (e.g., tube diameter, wall thickness), thermal conductivity of the tube material, and thermo physical properties of the fluids. Nominal or mean values of these parameters are used in the design calculations. However, uncertainties in these parameters prevent us from predicting the exact performance of the unit. The effect of the uncertainties is mostly in the performance degradation in service. Hence, there is an imperative need to consider all the uncertainties and to critically evaluate them and correctly predict the thermal performance of a heat exchanger. This is particularly true for critical applications. In thermal design of heat exchangers there are presently many stages in which assumptions in mathematical solution of the design problem are being made. Accumulation of these assumptions (e.g. use of mean values) may introduce variations in design as large as the uncertainties introduced in heat-transfer and flow friction correlations. The designer needs to understand where these inaccuracies may arise, and strive to eliminate as many sources of error as possible by choosing design configurations that avoid such problems at source. Heat Exchanger Thermal Design Problem referred to as the rating and sizing problems (Parag Mishra and Dr Manoj Arya, 2016)

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INTRODUCTION

Heat exchangers are equipment that transfers heat from one medium to another. An air cooled heat exchanger, or ACHE, is simply a pressure vessel which cools a circulating fluid within finned tubes by forcing ambient air over the exterior of the tubes (CFD, 2015).

*Corresponding author: Parag Mishra

Department of Mechanical Engineering, PhD Scholar, AISECT University Bhopal, MP India.

A heat exchanger is a heat-transfer devise that is used for transfer of internal thermal energy between two or more fluids available at different temperatures.

In most heat exchangers, heat transfer between fluids takes place through a separating wall or into and out of a wall in a transient manner. In many heat exchangers, the fluids are separated by a heat transfer surface, and ideally they do not mix or leak.

Types of draft in air cooled heat exchangers

There are many similar configurations by different manufacturers; however most of these are a derivative of one of these types. The most common type of air cooler is the horizontal coil with horizontal fan and vertical air flow. This type is typically driven by an electric motor drive attached to the fan through v-belts to allow for speed reduction between the motor and the fan. The normal application for these models are in plants or refineries where electric power is available, and where the cooler is installed away from other equipment to allow adequate air flow around the air cooler. This model is built in both induced draft and forced draft configurations (Parag Mishra, 2015).

Forced Draft ACHE

The most economical and most common style of air cooler is the forced draft ACHE, uses axial fans to force air across the fin tube bundle. The fans are positioned below the bundle thus not exposing the mechanical sections to the hot exhaust airflow. The forced draft air cooler also simplifies future plant expansion by providing direct access to bundle for replacement. Structural disassembly is not required. Forced Draft – fans are positioned below the tube bundle and force air across the fin tubes (Parag Mishra, 2015). A subset of the forced draft unit is called a "Winterized" unit. Here, a forced draft unit is outfitted with one or more methods to control the process fluid temperature leaving the ACHE. This type of unit is typically found in colder climates but is also used in hotter climates for process fluids with high viscosities and/or high pour points (Parag Mishra, 2015).

Induced Draft ACHE

The second most economical and most common style air cooler is the induced draft ACHE. This design uses axial fans to pull air across the fin tube bundle. The fans are positioned above the bundle thus offering greater control of the process fluid and bundle protection due to the additional structure. Lower noise levels at grade are another benefit. The induced draft air cooler does require some structural disassembly if bundle replacement is required. Induced Draft – fans are positioned above the bundle and pull across the fin tubes. Induced draft coolers offer improved air distribution and protection of the tube bundle from the elements (Parag Mishra, 2015).

Problems with Heat Exchangers in Low-Temperature Environments

Heat Exchanger is designed on the basis of hot fluid temperature, cold fluid temperature & ambient temperature, but in practical sense, the ambient temperature changes throughout the year. In that case, the fluid in heat exchanger freezes. In extremely cold environments, overcooling of the process fluid may cause freezing. This may lead to tube burst, and hence freeze protection is required to prevent plugging or damage to the tubes. For this, we can use steam coil in Heat Exchanger for heating the working fluid (Parag Mishra, 2016).

The process parameters/boundary conditions for thermal design of Air Cooled heat Exchanger are

- Flow rate of hot & cold fluid
- Inlet & outlet temperature of hot & cold fluid
- Inlet temperature of cold fluid
- Allowable pressure drop

Dimensions of Air Cooled Heat Exchanger

Dimension of Air Cooled Heat Exchanger is based on plot area or land area. Important dimensions of Air Cooled Heat Exchanger includes-

- Total Plot area
- Bays in parallel per unit
- Bundles parallel per bay
- Bundle width
- Length of tube
- Number of rows
- Number of fan/bay
- Fan Diameter

Computational Software for Using Thermal Design of Air Cooled Heat Exchanger

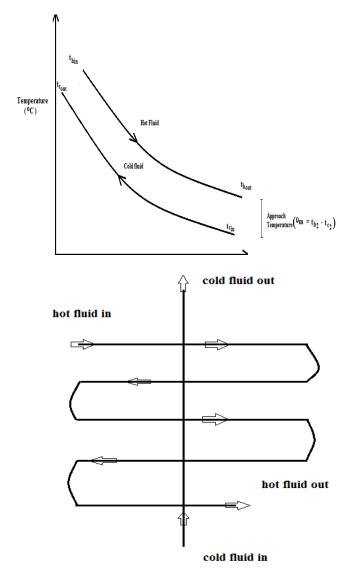
Reflecting the growing trend of using computers for design and teaching, recent heat transfer texts incorporate computer software for the design and optimization of heat exchangers. These software are written to reinforce fundamental concepts and ideas and allow design calculations for generic configurations with no reference to design codes and standards used in the heat exchanger industry. For actual engineering applications, most heat exchangers are designed using commercially available software such as those developed by co-operative research organizations such as Heat Transfer and Fluid Flow Service (HTFS) and Heat Transfer Research Inc. (HTRI) and by computer service companies such as B-JAC International. These programs offer design and cost analysis for all primary heat exchanger types and incorporate multiple design codes and standards from the American Society of Mechanical Engineers (ASME), Tubular Exchangers Manufacturers Association (TEMA) and the International Standards Organization (ISO). These are user-friendly computer software developed for the thermal and hydraulic design of heat exchangers. (LEONG and TOH, 1998)

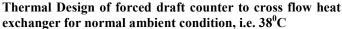
Approach Temperatures The approach temperatures are the difference between the Outlet Temperature of one stream and the Inlet Temperature of the other stream. Although each application will have two approach temperatures, typically it is obvious which one is important from a design standpoint. (Parag Mishra and Dr manoj Arya, 2016)

Objectives

• The main objective of this master thesis is to give the idea for thermal design of Forced Draft Counter to Cross Flow Air Cooled Heat Exchanger at normal ambient temperature, as there are lots of problems associated, while designing an Air Cooled Heat Exchanger

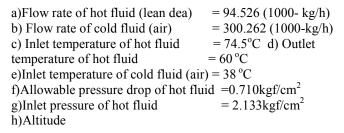
- In this research paper we analyze the effect of ambient temperature on Forced Draft Counter to Cross flow Air Cooled Heat Exchanger. Here, we have taken the temperature of surrounding air, as 38°C. Here, we are studying the performance & design analysis of Air Cooled heat exchanger at normal ambient temperature.
- To give the thermal design & procedure of Air cooled heat exchanger counter to cross flow at normal ambient temperature
- To discuss the various challenges while designing the Counter to Cross Flow Heat Exchanger.

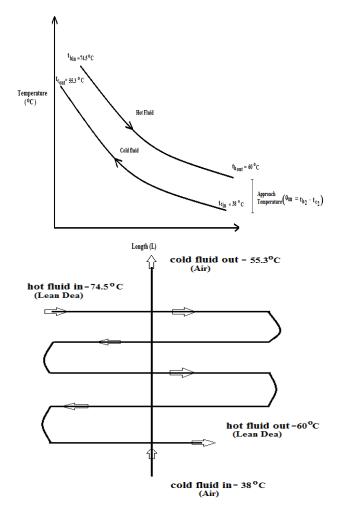




In this we have done the thermal design & performance analysis of forced draft counter to cross flow cooled air heat exchanger at normal ambient conditions, so we have taken 38^oC temperature for designing & performance analysis of Air Cooled Heat Exchanger. The most important parameter, while taking into consideration of designing Air Cooled Heat Exchanger is permissible /minimum tube skin temperature. In this forced draft counter to cross flow air cooled heat exchanger, the process fluid is lean dea. The pour point of any fluid can be defined as that point, when fluid ceases to flow i.e. fluid start freeze on this temperature In this case, the hot fluid lean dea enters in the Air Cooled Heat Exchanger &the hot fluid is cooled by passing the ambient air with the help of fans, which directs the air in tube bundles & fluid cools down.

For normal atmospheric conditions, i.e. ambient temperature is 38°C, the process parameters are





Nomenclature

Hot fluid (lean dea) enters in Air Cooled Heat Exchanger $=t_{hin} =74.5^{\circ}C$

Hot fluid (lean dea) leaves the Air Cooled Heat Exchanger = $t_{hout} = 60 \ ^{o}C$

Cold fluid (air) enters in Air Cooled Heat Exchanger $= t_{cin} = 38 \ ^{\circ}C$

Cold fluid (air) leaves the Air Cooled Heat Exchanger	=
$t_{cout} = 55.3 ^{\circ}\text{C}$	
Change in hot fluid (lean dea) temperature Δt_h	=
t_{hin} - $t_{hout} = 74.5^{\circ}$ C-60 °C=14.5 °C	
Change in cold fluid (air) temperature Δt_c	=
t_{cout} - t_{cin} =55.3 °C-38 °C =17.3 °C	
Approach Temperature = $m1 = t_{hout} \cdot t_{cin} = 60 ^{\circ}\text{C} \cdot 38 ^{\circ}\text{C}$	= 22
°C	
Approach Temperature $m_2 = t_{hin} - t_{cout} = 74.5^{\circ}C - 55.3^{\circ}C$	C
=19.2 °C	

There are two different approach temperatures, but in counter to cross flow heat exchanger, we consider the Approach Temperature $= m_1 = t_{hout} \cdot t_{cin}$

Only this approach temperature is important, while designing the forced draft counter to cross flow heat exchanger.

By using thermal design software we found the following properties of hot fluid (lean dea) & cold fluid (Air) Stream properties of hot fluid side fluid (lean dea)

Rating-Horizontal	air-cooled heat e	xchanger fo	orced draft	countercurr	ent to cross		KH Units
Hot Tubeside Flui			Inlet			Outlet	
Fluid name				Lear	1 DEA		
Temperature	(C)		74.50			60.00	
Pressure	(kgf/cm2A)		2.133			1.559	
Weight fraction va	por ()		0.0000			0.0000	
Vapor Pro	perties						
Density	(kg/m3)						
Viscosity	(cP)						
Conductivity	(kcal/hr-m-C)						
Heat capacity	(kcal/kg-C)						
Molecular weight	()						
Liquid Pro	operties						
Density	(kg/m3)		1002.20			1011.50	
Viscosity	(cP)		0.7600			1.0400	
Conductivity	(kcal/hr-m-C)		0.4428			0.4338	
Heat capacity	(kcal/kg-C)		0.9150			0.9090	
Molecular weight	()		0			0	
Latent heat	(kcal/kg)						
Surface tension	(dyne/cm)		0.0000			0.0000	
Molar Com	position	Vapor	Liquid	K-Value	Vapor	Liquid	K-Valu
1 [New User-De	efined]						-

Stream properties of cold outside fluid (Air)

Rating-Horizontal a	air-cooled heat ex	changer forced draft	countercurre		KH Units
Cold Outside Flui	d	Inlet		Outlet	
Fluid name					
Temperature	(C)	38.00		55.31	
Pressure	(kgf/cm2A)	1.031		1.030	
Weight fraction va	oor ()	1.0000		1.0000	
Vapor Pro	perties				
Density	(kg/m3)	1.1324		1.0727	
Viscosity	(cP)	0.0190		0.0197	
Conductivity	(kcal/hr-m-C)	0.0234		0.0245	
Heat capacity	(kcal/kg-C)	0.2404		0.2407	
Molecular weight	()	28.96		28.96	
Liquid Pro	perties				
Density	(kg/m3)				
Viscosity	(cP)				
Conductivity	(kcal/hr-m-C)				
Heat capacity	(kcal/kg-C)				
Molecular weight	()				
Latent heat	(kcal/kg)				
Surface tension	(dyne/cm)				
Molar Com	position	Vapor Liquid	K-Value	Vapor Liquid	K-Valu

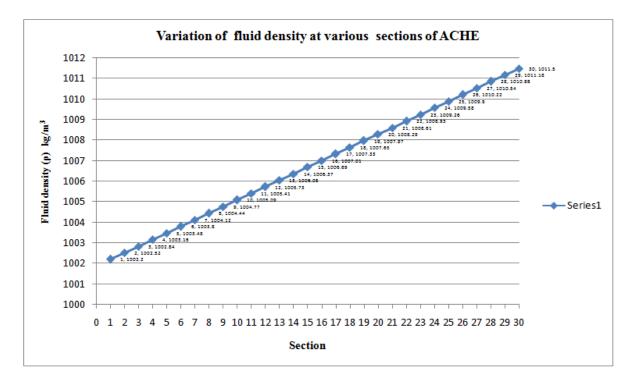
Physical properties of hot tube side (lean dea) at various sections of forced draft counters to cross flow Air Cooled heat exchanger at normal ambient temperature

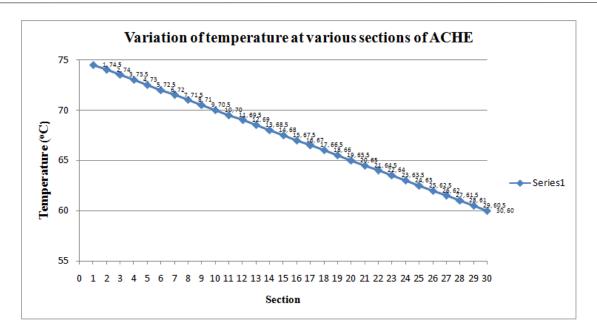
Properties Profile Monitor

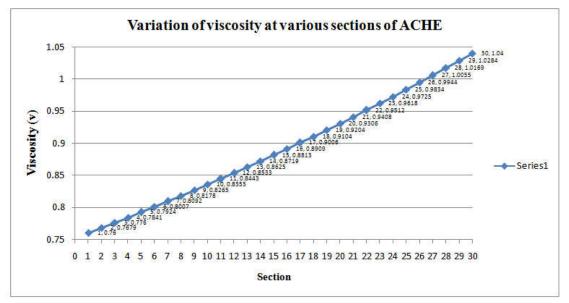
										MK	H Units
Rating-Horizontal air-cooled heat exe	char	iger force	d draft cou	Intercurre	nt to cross	flow					
Physical Properties Profile: Hot To											
Reference pressure, (kgf/cm2A)	(P1	= 2.133)									
	(P)	1	2	3	4	5	6	7	8	9	10
Temperature, (C)	1	74.50	74.00	73.50	73.00	72.50	72.00	71.50	71.00	70.50	70.00
Heat duty/flow rate, (kcal/kg)	1	0.0000	0.4575	0.9148	1.3721	1.8292	2.2863	2.7432	3.2001	3.6568	4.1134
Weight fraction vapor	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Liquid Properties											
Density, (kg/m3)	1	1002.20	1002.52	1002.84	1003.16	1003.48	1003.80	1004.12	1004.44	1004.77	1005.09
Viscosity, (cP)	1	0.7600	0.7679	0.7760	0.7841	0.7924	0.8007	0.8092	0.8178	0.8265	0.8353
Thermal conductivity, (kcal/hr-m-C)	1	0.4428	0.4425	0.4422	0.4419	0.4416	0.4413	0.4410	0.4406	0.4403	0.4400
Enthalpy, (kcal/kg)	1	0.0000	-0.4575	-0.9148	-1.3721	-1.8292	-2.2863	-2.7432	-3.2001	-3.6568	-4.1134
Specific heat, (kcal/kg-C)	1	0.9150	0.9148	0.9146	0.9144	0.9142	0.9140	0.9138	0.9136	0.9133	0.9131
Surface tension, (dyne/cm)	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Critical pressure, (kgf/cm2A)	1	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Latent heat, (kcal/kg)	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

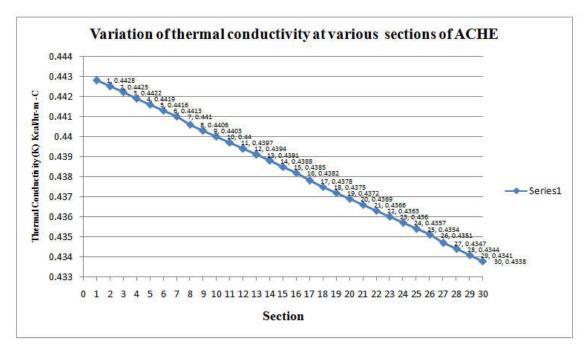
			Propert	ies Pro	file Mo	nitor					
Dating Harizantal air apolad baat av	obor	ager force	d droft oo	untorourro	at to propo	flow				МК	H Units
Rating-Horizontal air-cooled heat exe Physical Properties Profile: Hot Tu				untercurre		now					
Reference pressure, (kgf/cm2A)		= 2.133)									
	(P)	11	12	13	14	15	16	17	18	19	20
Temperature, (C)	1	69.50	69.00	68.50	68.00	67.50	67.00	66.50	66.00	65.50	65.00
Heat duty/flow rate, (kcal/kg)	1	4.5700	5.0264	5.4827	5.9389	6.3950	6.8510	7.3070	7.7628	8.2185	8.6741
Weight fraction vapor	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Liquid Properties											
Density, (kg/m3)	1	1005.41	1005.73	1006.05	1006.37	1006.69	1007.01	1007.33	1007.65	1007.97	1008.29
Viscosity, (cP)	1	0.8443	0.8533	0.8625	0.8719	0.8813	0.8909	0.9006	0.9104	0.9204	0.9306
Thermal conductivity, (kcal/hr-m-C)	1	0.4397	0.4394	0.4391	0.4388	0.4385	0.4382	0.4378	0.4375	0.4372	0.4369
Enthalpy, (kcal/kg)	1	-4.5700	-5.0264	-5.4827	-5.9389	-6.3950	-6.8510	-7.3070	-7.7628	-8.2185	-8.6741
Specific heat, (kcal/kg-C)	1	0.9129	0.9127	0.9125	0.9123	0.9121	0.9119	0.9117	0.9115	0.9113	0.9111
Surface tension, (dyne/cm)	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Critical pressure, (kgf/cm2A)	1	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Latent heat, (kcal/kg)	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000

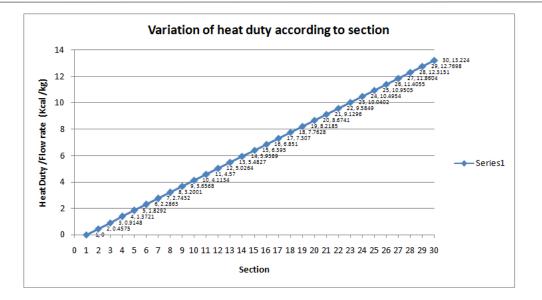
			Propert	ies Pro	file Moı	nitor					
Rating-Horizontal air-cooled heat exc	char	nger force	d draft cou	untercurre	nt to cross	flow				MK	H Units
Physical Properties Profile: Hot Tu	ubes	side (Lea	n DEA)								
Reference pressure, (kgf/cm2A)	(P′	1= 2.133)									
	(P)	21	22	23	24	25	26	27	28	29	30
Temperature, (C)	1	64.50	64.00	63.50	63.00	62.50	62.00	61.50	61.00	60.50	60.00
Heat duty/flow rate, (kcal/kg)	1	9.1296	9.5849	10.0402	10.4954	10.9505	11.4055	11.8604	12.3151	12.7698	13.2240
Weight fraction vapor	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Liquid Properties											
Density, (kg/m3)	1	1008.61	1008.93	1009.26	1009.58	1009.90	1010.22	1010.54	1010.86	1011.18	1011.50
Viscosity, (cP)	1	0.9408	0.9512	0.9618	0.9725	0.9834	0.9944	1.0055	1.0169	1.0284	1.0400
Thermal conductivity, (kcal/hr-m-C)	1	0.4366	0.4363	0.4360	0.4357	0.4354	0.4351	0.4347	0.4344	0.4341	0.4338
Enthalpy, (kcal/kg)	1	-9.1296	-9.5849	-10.040	-10.495	-10.951	-11.406	-11.860	-12.315	-12.770	-13.224
Specific heat, (kcal/kg-C)	1	0.9109	0.9107	0.9104	0.9102	0.9100	0.9098	0.9096	0.9094	0.9092	0.9090
Surface tension, (dyne/cm)	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000
Critical pressure, (kgf/cm2A)	1	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000	0.000
Latent heat, (kcal/kg)	1	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000	0.0000











RESULTS

	C	Dutput S	ummary					
Rating-Horizontal air-cooled	d heat exchange	er forced dra	ft countercur	rent to cro	ssflow		MKH Un	nits
Process C	onditions		Out	side		Tubesi	do	
Fluid name	onunions		Out	Side		Lean DEA	ue	
Fluid condition				Sens. Ga			Sens. Liquid	
Total flow rate	(1000-kg/hr)			300.26			94.526	
Weight fraction vapor, In/O	· · · ·		1.000	1.00		0.000	0.000	
Temperature, In/Out	(Deg C)		38.00	55.3		74.50	60.00	
Skin temperature, Min/Max	(Deg C)		50.49	65.43		57.16	71.83	
Pressure, Inlet/Outlet	(kgf/cm2A)		1.031	1.03		2.133	1.559	
Pressure drop, Total/Allow	,	(kgf/cm2)	14.141	0.00		0.575	0.710	
Midpoint velocity	(m/s)		1.1.1.1	6.8		0.575	1.48	
- In/Out	(m/s) (m/s)			0.0.	´	1.49	1.53	
Heat transfer safety factor	()				1	1.40	1.00	
Fouling	(m2-hr-C/kcal)			0.00000			0.000500	
- Connig			Exchange	er Perform			0.000000	
Outside film coef	(kcal/m2-hr-C)		40.11	Actua		(kcal/m2-hr-C)	21.814	
Tubeside film coef	(kcal/m2-hr-C)		4508.25	Regui	red U	(kcal/m2-hr-C)		
Clean coef	(kcal/m2-hr-C)		31.113	Area		(m2))
Hot regime	(,		ens. Liquid	Overc	lesign	(%)		
Cold regime			Sens. Gas			Tube Geome		
EMTD	(Deg C)		20.4	Tube	tvpe		High-finned	
Duty	(MM kcal/hr)		1.249	Tube		(mm)	•	
	Unit Geo			Tube	ID	(mm)		
Bays in parallel per unit			1	Lengt		(mm)		
Bundles parallel per bay			2		atio(ou	()		
Extended area	(m2)		2811.99	Layou		()	Staggered	
Bare area	(m2)		123.118	Trans		(mm)		
Bundle width	(mm)		1276.	Long	•	(mm)		
Nozzle	()	Inlet	Outlet	U U	er of p	· · ·		
Number	()	1	1		er of ro			
Diameter	(mm)	131.750	131.750	Tubeo		())
Velocity	(m/s)	0.96	0.95)dd/Even ()		16
R-V-SQ	(kg/m-s2)	925.32	916.81		materia	()	Carbon steel	
Pressure drop	(kgf/cm2)	5.190e-3	3.273e-3	1000	matom	Fin Geome		
	Fan Geo		0.27000	Туре			Plain round	
No/bay	()	,	2	Fins/l	enath	fin/meter		
Fan ring type			30 deg	Fin ro		mm		
Diameter	(mm)		2286.	Heigh		mm		
Ratio, Fan/bundle face area	()		0.40	- 5	thickne			
Driver power	. (kW)		10.42	Over		mm		
Tip clearance	(mm)		11.430	Efficie		(%)		
Efficiency	(%)		65		-	n/bare) ()		
Airside Velocities		Actual	Standard	Mater	ial	Aluminum	1060 - H14	
Face	(m/s)	3.61	3.40			Thermal Resist	ance, %	
Maximum	(m/s)	6.69	6.31	Air			54.39)
Flow (100 m3/min)	44.192	41.654	Tube			13.25	i
Velocity pressure	(mmH2O)	4.658		Foulir	ıg		29.89	
Bundle pressure drop	(mmH2O)	12.306		Metal			2.47	
Bundle flow fraction	()	1.000		Bond			0.00	
Bundle	87.02		Airside Pres					4.63
Ground clearance	0.00	Fan guard		0.53		ail screen		0.00
Fan ring	1.97	Fan area b	lockage	5.8	5 St	eam coil		0.00

		F	Final Resu	llts	5			
		due ft e e u						MKH Unit
Rating-Horizontal air-cooled heat exch	anger forced Proces			cros rsic			Tubeside	
Fluid name	FICCES	S Dala	AI	1510	1e	Lean		
Fluid condition					Sens. Gas	Loan	DER	Sens. Liqui
Total flow rate	(10)	00-kg/hr)			300.262			94.52
Weight fraction vapor, In/Out	(10)	()	1.000		1.000		0.000	0.00
Temperature, In/Out		(Deg C)	38.00		55.31		74.50	60.0
Skin temperature, Min/Max		(Deg C)	50.49		65.43		57.16	71.8
Wall temperature, Min/Max		(Deg C)	50.49		65.43		56.94	71.6
Pressure, In/Out	(k	gf/cm2A)	1.031		1.030		2.133	1.55
	- · ·	kgf/cm2)	14.141		0.000		0.575	0.71
Pressure Drop, A-frame reflux section		kgf/cm2)						0.11
Velocity - Midpoint	((m/s)	6.85				1.48	
- In/Out		(m/s)	0.00				1.49	1.5
Film coefficient, Bare/Extended	(kcal/i	m2-hr-C)	916.06		40.11	4	1508.25	
Mole fraction inert	(()					· · · · · ·	
Heat transfer safety factor		()			1			
Fouling resistance	(m2-h	r-C/kcal)			0.000000			0.00050
•	`	,	Overall Perf	forn	nance Data			
Overall coef, Design/Clean/Actual	(kcal/i	m2-hr-C)	21.768	1	31.113 /		21.814	
Heat duty, Calculated/Specified	•	1 kcal/hr)	1.2492	1	1.2500			
Effective mean temperature difference		(Deg C)	20.41					
Bays in parallel/unit Extended area/unit Extended area/bundle	() (m2) (m2)		2811.99 1405.99		Bundles in paralle Bare area/unit Bare area/bundle	5	(m2) (m2)	123.11 61.55
Tubepasses/Tuberows	(112)	4 /	6		Number of tubes/	hundle	(1112)	9
Tubecount, Odd rows/Even rows	()	17 /	16		Edge seals		()	Ye
Bundle width	(mm)		1276.		Fan guard		()	Ye
Clearance	(mm)		9.525		Louvers		()	Ye
Header depth	(mm)		101.600		Steam coil		()	N
Header Box	()				Hail screen		()	N
- Plate thickness	(mm)		25.400		Tube support info	rmation		
- Tubesheet thickness	(mm)		34.925		- Number		()	
Plenum type	()		Tapered		- Width		(mm)	25.40
Weight/Bundle	(kg)		3640		Orientation (from	horiz.)	(deg)	0.0
Structure weight	(kg)		3438		Tubeside volume	,	(L)	386.
Total weight, Dry / Wet	(kg)		13238	/	14011			
_adder/walkway weight	(kg)		2520		Cost Factor		()	47.356
			Tube In	for	mation			
Straight length	(mm)		8000.		Tube type			High-finne
Unfinned length	(mm)		36.000		Unheated length		(mm)	171.45
Layout	()		Staggered		Area ratio (fin/bar		()	22.839
Transverse pitch	(mm)		75.000		Fins per unit leng	th	(fin/meter)	433.
₋ongitudinal pitch	(mm)		64.950		Fin root diameter		(mm)	27.00
Tube form	()		Straight		Fin height		(mm)	15.07
Dutside diameter	(mm)		25.400		Fin thickness at b		(mm)	0.40
nside diameter	(mm)		21.184		Fin thickness at ti	р	(mm)	0.18
Area ratio (out/in)	()		27.3853		Fin type		()	Plain roun
Over fin dienseter	(mm)		57.150		Fin efficiency		(%)	79.
Over fin diameter								
Tube material Fin material			Carbon steel 1060 - H14		Internal tube type			Non

		Final Res	ults		
Rating-Horizontal air-cooled	heat exchanger force	d draft countercurrent t	o crossflow		MKH Units
¥	Airside Velocities		0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Actual	Standard
	Anside velocities	1.	m/n)		Standard 3.40
Face velocity		•	n/s) n/s)	3.61 6.69	3.40 6.31
Maximum velocity		•	,		
Volumetric flow		(100 m3/r	,	44.192	41.654
Maximum mass velocity		(kg/s-		7.575	
Air humidity			(%)		
Volumetric flow per fan at fa	n inlet	(100 m3/r		22.096	
Velocity at fan inlet		() (1	n/s)	8.97	
		Fan Description	and Fan Power		
Number of fans per bay			()		2
Diameter			(mm)		2286.
Tip clearance			(mm)		11.430
Ratio, fan area to bay face a	rea		()		0.40
Fan ring type			()		30 deg
	an guard		(%)		95
	nail screen		(%)		0
Ratio, ground clearance to fa	an diameter		()		
Percent blockage, other obs			(%)		5
Bundle pressure drop/ Veloc			(mmH2O)	12.306 /	4.658
Fan and drive efficiency	.,		(%)		65
Motor power per fan-design	air temperature		(kW)		10.42
Motor power per fan-minimu			(kW)		0.00
Ambient temperature, maxin			(Deg C)	-17.78 /	-17.78
		Two-Phase F			
Method	Inlet	Center	Outlet	Mix F	
Method	lillet	Center	Outlet		
Bundle flow fraction	()	1.000			
Heat Transfer an	d Pressure Drop Pa	rameters		Tubeside	Outside
Midpoint j-factor			()		0.0062
Heat transfer		Wall Correction	()	0.9912	0.9865
		Row Correction	()		1.0000
Midpoint f-factor			()	0.0068	0.1973
Pressure drop		Wall Correction	()	1.0079	1.0091
		Row Correction	()		1.0012
Reynolds number		Inlet	()	41514	10787
		Midpoint	()	34313	10591
		Outlet	()	31602	9749
Fouling layer thickness			(mm)	0.000	0.000
Input minimum velocity			(m/s)	0.000	0.000
Input maximum velocity			(m/s)		
Input minimum wall tempera	iture		(III/S) (Deg C)		
Input maximum wall tempera			(Deg C)		
	Thermal R	esistance (Pe	ercent)		Over
Air	Tube	Fouling	Metal	Bond	Design
54.39	13.25	29.89	2.47	0.00	0.21
		Airside P	ressure Drop	Percent)	
Across bundle		87.02	Other obstruction		5.85
Fan ring		1.97	Steam coil		0.00
Fan guard		0.53	Louvers		4.63
Ground clearance		0.00	2001010		4.00
	zzle (Perpendicular)		Inlet	Outlet	
Number of nozzles	reipenuicular)	()	1	1	
Diameter		(mm)	131.750	131.750	
Velocity				0.95	
		(m/s)	0.96		
Nozzle R-V-SQ		(kg/m-s2)	925.32	916.81	
Pressure drop		(kgf/cm2)	5.190e-3	3.273e-3	

Conclusion and Outcome

The most important parameter, while taking into consideration for designing the Forced Draft Counter to cross flow Air Cooled Heat Exchanger is tube skin temperature. In this Forced Draft Counter to cross flow Air Cooled Heat Exchanger, the process fluid is lean dea Here, the air acts as a cold fluid & lean dea acts as a hot fluid. The hot fluid lea dea loses its heat from 74.5°C to 60°C& cold fluid air gains the heat from 38°Cto 58.31°C, during heat exchanging process. By studying the various properties of lean dea, we come to know that, the pour point of lean dea is 8°C & by studying API 661 guidelines for designing of Air Cooled Heat Exchanger, the minimum tube skin temperature is equal to the pour pint of fluid +9°C API Margin. i.e. Permissible/ minimum tube skin temperature = pour point of fluid (lean dea) +9 °C (API Margin) = 8°C +9°C = 17 °C By studying the properties of lean dea we come to know that the tube skin temperature at 38

 $^{\circ}$ C is 57.16 $^{\circ}$ C. At 38 $^{\circ}$ C the permissible tube skin temperature is 57.16 $^{\circ}$ C, which is far greater than the permissible tube skin temperature (17 $^{\circ}$ C), So, the design & performance of Forced Draft Counter to Cross Flow Air Cooled Heat Exchanger is safe. In this ambient conditions, there is no need of steam coil because at this temperature, the fluid in the heat exchanger does not freeze, hence there is not a problem.

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