



RESEARCH ARTICLE

BEHAVIOUR OF HIGH PERFORMANCE FIBRE REINFORCED CONCRETE LAYERED BEAMS

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ARTICLE INFO

Article History:

Received 27th August, 2017
Received in revised form
04th September, 2017
Accepted 29th October, 2017
Published online 30th November, 2017

Key words:

Layered beams,
M20,
M60,
M60/M20,
M60/M20/M60,
Fiber Reinforced High Performance
Concrete (FRHPC),
Normal strength concrete (NSC),
Steel fibers,
Energy absorption capacity,
Toughness,
Ductility index,
Cracking moment,
Flexural strength.

ABSTRACT

The Layered reinforced cement concrete beams can be analyzed using conventional methods for composite element consisting of fibre reinforced high performance concrete (FRHPC) and Normal strength concrete (NSC) to improve the efficiency of concrete matrix of different layered flexural member. A beam is a flexural member which provides support to the slab and vertical walls, as flexural members plays an important role in the structural system hence specific attention has been given to study affect of different concrete matrix in the form different concrete layers on behavior of flexural member under static loading. In reinforced cement concrete beam generally consists of two zones i.e., compression zone at top and tension zone at bottom. As concrete is weak in tension, steel is introduced in the tension zone to take up the tension, but as strength of concrete is ignored in tension zone with respect to compression zone. As the concrete in the tension zone of the section contributes little to the beam load bearing capacity. Hence in the present experimental investigation the tension layer is made of normal strength concrete while the compression layer is made of fibre reinforced high performance concrete and also combination of both. The possibility of such scheme is practical a new innovative construction technology so a higher concrete strength is required in the beam's compression zone to withstand rather large bending moments under serviceability. The research is aimed at experimental investigation focused on two layered as well as three layered test beams specimens consisting of High Performance Fibre Reinforced Concrete (HPFRC) and Normal Strength Concrete (NSC) in tension zone with varying depth to optimize and to improve the efficiency of layered concrete matrix (HPFRC and NSC) consisting of following grades of concrete with layered as M₂₀, M₆₀, M₆₀/M₂₀, M₆₀/M₂₀/M₆₀ to study energy absorption capacity, toughness, ductility index, cracking moment and consequently load carrying capacities of layered test beam specimens from Load-deflection curve to assess the enhancement in flexural strength and same is to be optimized with minimum use of FRHPC for layered beam concept.

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Citation: Srinivas, H. R. and Dr. Sadath Ali Khan Zai, 2017. "Behaviour of high performance Fibre reinforced concrete layered beams", *International Journal of Current Research*, 9, (10), 61245-61250.

INTRODUCTION

Concrete is a widely used construction material in civil engineering all over the world. Its history begins since cement was invented. Reinforced cement concrete is extensively used in the construction of variety of civil infrastructure applications including small and large buildings, houses, bridges, storage tanks, dams and numerous other types of structures. Two different concrete grade layers in single flexural member fall into the category of composite structures. The Study on the two-layer flexural member is logical development, consisting of fiber high performance concrete in a compression zone

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and normal strength concrete in the tensile zone, as flexural member is effective when the reinforced concrete (RC) section carries rather larger bending moments. The possibility of such scheme in practical at new constructions, when the beam span becomes longer and the service load increases, so a higher concrete strength is required in the beam's compression zone to withstand rather than to control large bending moments. As concrete in the tension zone of the section contributes little to the beam's load bearing capacity, this zone is made of normal strength concrete in the layered beam, with taking into consideration into economical advantage with higher strength. The concept of hybrid section in steel - concrete structures is not a new idea. Some of researchers (Salmon and Johnson, 1990) defined a hybrid girder as one that has either the tension flange or both flanges of steel section made with a higher

strength grade of steel than used for the web. Others (Bernard, 1998) defined hybrid concrete structures as structural elements consisting of new and old.

Literature review

Reinforced Concrete beams consisting of two concrete layers of different strengths fall into the category of composite structures and may therefore be analyzed using known methods for composite materials. When extending the hybrid concept to composite concrete members and due to advances in concrete technology, it is relatively easy to produce composite sections which possess high compressive strength, high ductility, high energy absorption and high tensile strength at the same time, these characteristics can be achieved by placing two or more different types or strengths of concrete layers together so that each layer is used to its best advantage and as a result, the concrete section becomes a "hybrid" section or the Layered concrete section. It was shown that these beams are effective when the design compressed zone depth corresponds to a case when the Reinforced Concrete section carries a maximum bending moment, but brittle failure of compressed concrete is avoided. High strength concrete is widely used in structures despite its relatively low tensile strength and weak deformation capability. Steel fibers increase the energy absorption of concrete and ductility of bending elements' sections. This feature is especially important for sections withstanding ultimate loads (including dynamic ones). Therefore, Steel Fibre High Strength Concrete becomes a material with high resistance to cracking and relatively high ductility. High Performance Concrete (HPC) is an engineered concrete possessing the most beneficial properties during fresh as well as hardened concrete stages. HPC is far superior to conventional cement concrete as the ingredients of High Performance Concrete contribute most optimally and efficiently to the various properties. (Lalit Rathee and Naveen Hooda, 2016) experimental studies on high strength fibre reinforced concrete subject to plastic shrinking cracks Polyester & polypropylene fibres are better than glass fibre, because differences in stiffness, low elastic modulus and these are much longer than glass fibres. The steel and polyester hybrid combination is performed better than other combinations. are reduces the crack width, (Somasekharaih, Mahesh Sajjan, Nelson Mandela, 2015) study flexural behaviour of high strength steel fibre reinforced concrete beam were tested under two point load condition The test result indicates that the optimum fibre volume fraction was 1%. fraction resulted in higher load carrying capacity and enhanced ductility. (Venkatesan *et al.*, 2015) Design method for two-layer beams consisting of normal and fibered high strength concrete". They analyzed two-layer concrete beam consisting the compressed zone of such beam section is made of high strength concrete (HSC) and the tensile one of normal strength concrete (NSC). research has been carried out on the ductility parameters, Poisson coefficient, energy dissipation (Iskhakov *et al.*, 2014) Two-layer high-performance RC beams were used in the traffic (longitudinal) direction of long-span bridges for studies concrete grade variation in tension and compression zones of RCC beams. (Iskhakov and Ribakov, 2013) studied based on results of theoretical investigations and tests that showed high efficiency of such beams, carrying rather big bending moments As concrete in the tension zone of the section contributes little to the beam's load bearing capacity, this zone is made of NSC (Holschemacher, *et al.*, 2012, Iskhakov *et al.*, 2007, Eramma *et al.*, 2011) two-layer bending

pre-stressed beam consisting of steel fibered High strength concrete in compressed zone and normal strength concrete in tensile zone" The HSC layer made of steel fiber will allows improving the beams compressed zone plastic properties. From the literature review a limited research work has been reported on development and optimization of layered concrete (or) the hybrid concrete in flexural structural member. Hence attempt has been made in the present experimental investigation on two-layers and three layers test beam specimens consisting of FRHPC (M60+steel fibre) and NSC (M20) concrete matrix in tension zone and compression zone with varying thickness of FRHPC and NSC in flexural member to enhance the load carry capacity to obtain Maximum flexural Strength and same is to be optimized with economical.

Experimental investigation

Materials and mix proportions

In this present experimental investigation Ordinary Portland Cement of 53 Grade Ultra Tech (Birla Super) is used. To ascertain the physical characteristics of the cement, tests were conducted in accordance with the Indian standards confirming to IS-12269:1987. Fractions of fine aggregates passing through 4.75 mm sieves and entirely retained on 150 μ sieve are used. The test on fine aggregate was conducted in accordance with IS: 650-1966 & IS: 2386-1968 to determine specific gravity and fineness modulus. The Fine aggregate satisfied the requirement of grading Zone II as per IS: 383 – 1970 (Reaffirmed 2007). Crushed Granite stone with Two different sizes of coarse aggregates were used, 60 % of coarse aggregate passing 20 mm sieve size and retained on 12.5mm sieve, remaining 40% of coarse aggregate passing 12.5 mm sieve size and retained on 10 mm sieve were used. The tests on coarse aggregate were conducted in accordance with IS 2386-1963 to determine specific gravity and fineness modulus. For mix proportioning of High Performance Concrete, Glenium ACE 30, with Poly carboxylic based ethers as Super Plasticizer as chemical admixture are used supplied by BASF India Ltd. Bangalore. Micro silica a dry powder available in densified form and Ground Granulated Blast Furnace Slag (GGBFS) is a dry powder as supplied by M/s Ultra Tech Aditya Birla Group India Pvt. Ltd, Bangalore are used as mineral admixtures in experimental program. Crimped end steel fibers having aspect ratio of 80, procured from Stewols India (Pvt) Ltd, Nagpur-Maharashtra. Ordinary potable water was used for mixing and curing purpose. To determine the mix proportions for M60 grade concrete (HPC), tests on trial mixes were carried out and was finally selected with required workability of 25-50mm slump, binder 8% of silica fume is replaced by weight of cement and 15% of GGBS, 0.8% of superplasticizer, 0.65% steel fibers by volume of concrete having aspect ratio of 80 were used. For 50mm slump value, the concrete mix proportional is obtained after trial mixes viz: Cement: Silica fume: GGBS: FA: CA: Water (1: 0.1: 0.19:0.99:2.55:0.38) and same is adopted for present experimental investigations. The hardened properties of concrete matrix used for Case A to Case F as shown in Table No.1.

Preparation of test specimens

In the present study, the behaviour of high performance fibre reinforced concrete layered beams under static test was carried out by casting and testing of 150x 230x1750mm rectangular test beam specimens with a different concrete

layers having steel reinforcements of 3 # 12 mm dia at bottom and 2 # 10 mm dia at top with two legs vertical shear of 8mm dia at 75mm c/c with HYSD bars (Figure No.1) conforming to IS: 1786 (grade Fe 500D), further the test beam specimens are divided into six categories (Case A to Case F) according to their material combination as listed below (Srinivas and Dr.Sadath Ali Khan Zai, 2017).

- **Case A**(Full M₂₀ grade concrete beam test specimen).
- **Case B**(Full M₆₀ grade concrete beam test specimen).
- **Case C** (Two layered M₆₀/M₂₀ grade concrete beam, M₆₀ depth is 50mm from top).
- **Case D**(Two layered M₆₀/M₂₀ grade concrete beam, M₆₀ depth is 70mm from top).
- **Case E**(layered M₆₀/M₂₀/M₆₀ grade concrete beam, M₆₀ depth is 50mm in upper layer, M₂₀ depth is 90mm in middle layer and M₆₀ depth is 90mm in bottom layer).
- **Case F**(layered M₆₀/M₂₀/M₆₀ grade concrete beam, M₆₀ depth is 70mm in upper layer, M₂₀ depth is 80mm in middle layer and M₆₀ depth is 80mm in bottom layer).

Table 1. Properties of Hardened Concrete (Srinivas and Dr.Sadath Ali Khan Zai, 2017)

Mix	Compressive strength (N/mm ²)	Split tensile strength (N/mm ²)	Flexural strength test (N/mm ²)
Case A	22.67	2.98	4.20
Case B	67.85	8.92	13.27
Case C	52.56	6.99	10.27
Case D	54.06	7.02	10.60
Case E	59.78	8.09	11.76
Case F	62.55	8.67	12.86

Test programme

The experimental programme consists of testing six series of test beam specimen under flexural loading, the loading arrangements and instrumentation are shown in figure No.2 simply supported reinforced concrete beam under two point loading at the one third of span is considered. The parameters under study are Energy absorption capacity, Toughness index, Ductility Factor, Cracking Moment. Test Beam specimens are designated as Beam1/CaseA, Beam2/CaseB, Beam3/CaseC, Beam4/CaseD, Beam5/CaseE, Beam6/CaseF, respectively and same is shown as in table no.2

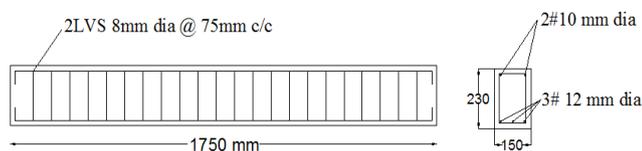


Figure 1. Reinforcement details

RESULTS

Flexural behaviour on layered test beams specimens

The behavior of the test beam specimens with constant tension reinforcements are tested under pure bending conditions for Case A to Case F (Beam 1 to Beam 6) and the test results of each test beam specimen with respect to deflection, cracking loads, energy absorption capacity, ductility index and

toughness index are presented in respective tables and bar charts. The experimental cracking moment, cracking loads are compared with corresponding moments and loads calculated as per IS 456:2000.

Table 2. Details description of Concrete Matrix for Case A to Case F

Sl. No.	Mix	Description	Cross Section of Test Beam Specimen
1	Case A	Beam with M ₂₀ grade concrete (Control specimen).	
2	Case B	Beam with M ₆₀ grade concrete.	
3	Case C	The beam with tension layer made of normal M ₂₀ grade concrete while the compression layer of 0.2857d made with high strength concrete beam.	
4	Case D	The beam with tension layer made of normal M ₂₀ grade concrete while the compression layer of 0.40d made with high strength concrete beam	
5	Case E	The beam with compression layer made of normal M ₂₀ grade concrete while the tension layer of 0.2857d made with high strength M ₆₀ grade concrete.	
6	Case F	The beam with compression layer made of normal M ₂₀ grade concrete while the tension layer of 0.40d made with high strength M ₆₀ grade concrete.	



Figure 2. Test Setup

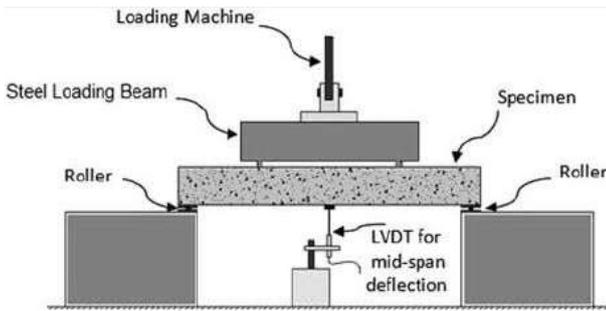


Figure 2. Test Setup

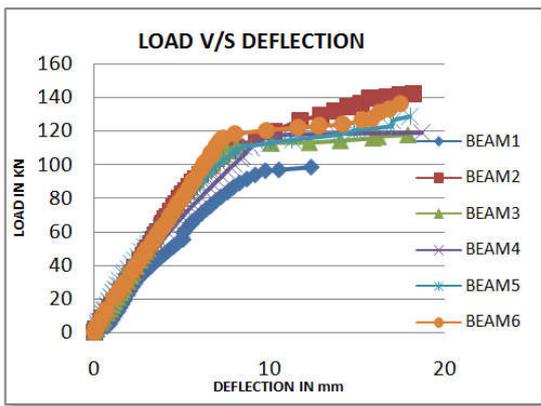


Figure 3. Combined Load-Deflection Curves for beam 1 to beam 6

Table 3. Experimental and Theoretical Values of First Crack Loads

Mix	Test Beam specimen	Experimental. first crack load in KN (E)	Theoretical. first crack load in KN (T)	Ratio T/E.
CASE A	B1	11.77	11.84	1.00
CASE B	B2	32.24	20.51	0.65
CASE C	B3	17.65	20.51	1.16
CASE D	B4	19.62	20.51	1.04
CASE E	B5	28.44	20.51	0.72
CASE F	B6	30.39	20.51	0.70

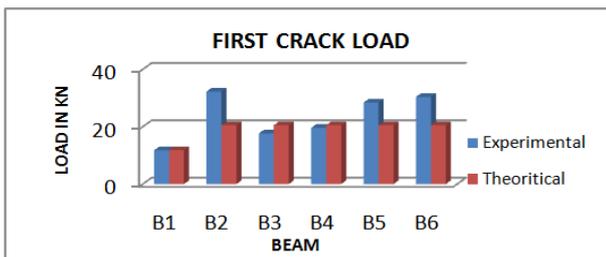


Figure 4. Comparison of Experimental and Theoretical First crack load

Table 4. Theoretical and experimental ultimate loads for all beams

Mix	Test Beam specimen	Expt. Ultimate load in KN (E)	Theoretical. Ultimate load in KN (T)	Ratio T/E.
CASE A	B1	98.51	62.62	0.63
CASE B	B2	142.54	187.92	1.31
CASE C	B3	117.98	187.92	1.59
CASE D	B4	119.12	187.92	1.57
CASE E	B5	128.25	187.92	1.46
CASE F	B6	134.25	187.92	1.39

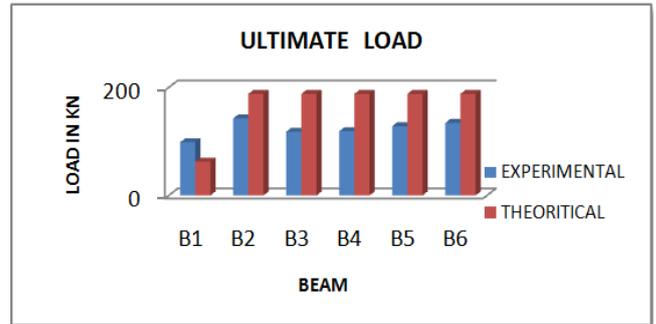


Figure 5. Comparison of Experimental and Theoretical Ultimate load

Load-deflection behaviour under static loading

Deflection is one of the important serviceability limit state to be satisfied in the design of concrete structures. Deflection of a beam primarily depends upon the type of loading, span, and moment of inertia of the section and modulus of elasticity of concrete. A significant overall property of a structural member is its response to load which is completely described by load deflection relationship and same is shown in Figure 3. It is observed that for all test beam specimens the curves shows linear variation up to first crack level and behave in a nonlinear way with further increase in load. The load deflection response can be idealized into three phases. In the first phase the load deflection plot is nearly straight for an uncracked section and the behavior is elastic. Phase two with a curved portion corresponds to deflection after the concrete in tension has cracked. At this stage the tensile steel will still be elastic. After the third phase either the steel or the concrete in compression or both become plastic and the strain increases rapidly up to failure.

First crack load

This is the load at which the first visible crack appears on the surface of the beam due to the development of tensile stresses. The experimental and theoretical loads at the first visible crack for all the six test beams specimens are shown in Figure 4 and Table 3.

Ultimate load

The term ultimate strength is the maximum load system which produces actual failure for the member under consideration. The experimental and theoretical ultimate loads for all the six test beams specimens are tabulated in Table 4 and Figure 5. and it is seen that the value of experimental ultimate load is more than that of respective theoretical ultimate load.

Energy absorption capacity

The Energy absorption capacity of given material can be obtained from the load versus deflection curve of the specimen. The value of Energy absorption capacity was computed from the area under the load deflection curve.

Table 5. Energy absorption capacity of different concrete beams

Mix	Test Beam specimen	Energy absorption capacity (kN-mm)
CASE A	B1	105.50
CASE B	B2	284.42
CASE C	B3	161.53
CASE D	B4	191.39
CASE E	B5	235.92
CASE F	B6	250.45

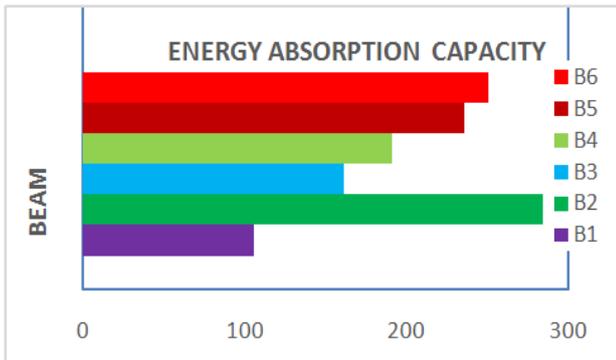


Figure 6. Energy Absorption capacity for all Beams

Toughness index

Toughness Index is defined as the ratio of area under the curve up to ultimate load to area under the curve up to first crack load. The value of toughness index for different beam specimen under investigation is given in table below.

$$\text{Toughness index} = \frac{\text{Area under the curve upto ultimate load}}{\text{Area under the curve upto first crack load}}$$

Table 6. Toughness index of different concrete beams

Test Beam specimens	Toughness Index
B1	10.25
B2	25.50
B3	14.39
B4	16.25
B5	19.25
B6	21.65

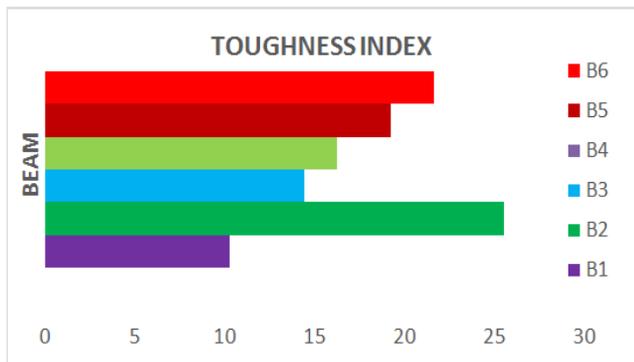


Figure 7. Toughness Index for all Beams

Flexural ductility index

Ductility is the measure of the element capacity to undergo inelastic behavior and absorb energy. Displacement ductility, μ_d , is defined as the ratio of deflection at ultimate moment to the deflection at first yield. In general, high ductility ratios indicate that a structural member is capable of undergoing large deflection prior to failure. Displacement ductility is given by

$$\mu_d = \delta_u / \delta_y$$

Table 7. Ductility Index

Mix	δ_y, mm	δ_u, mm	$\mu_d = \delta_u / \delta_y$
CASE A	9.176	12.368	1.347
CASE B	7.581	18.250	2.407
CASE C	9.592	17.942	1.879
CASE D	9.280	18.72	2.017
CASE E	8.512	18.024	2.114
CASE F	7.83	17.50	2.233

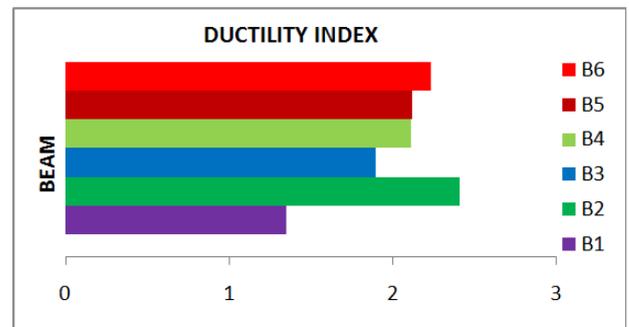


Figure 8. Ductility Index for all Beams

Table 8. Theoretical and Experimental Cracking Moment

Mix	Test Beam specimens	Exp. M_{CR} (kN-m)	Theo. M_{CR} (kN-m)	Ratio of M_{CR} Theo/Exp.
CASE A	B1	3.52	3.256	1.00
CASE B	B2	9.15	5.64	0.63
CASE C	B3	5.135	5.64	1.09
CASE D	B4	5.675	5.64	0.99
CASE E	B5	8.13	5.64	0.69
CASE F	B6	8.63	5.64	0.65

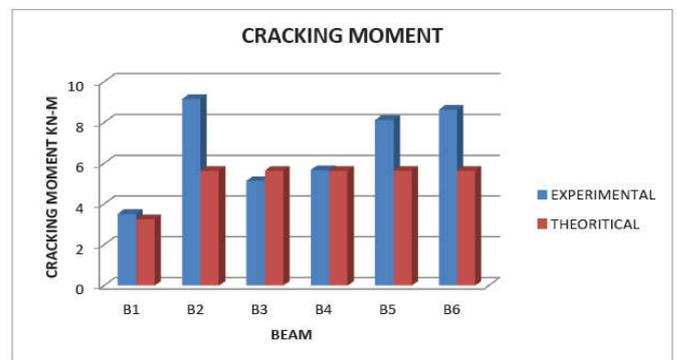


Figure 9. Cracking Moment for all Beams

Cracking moment

The Table 8 shows the observed moments at first crack, $M_{cr(\text{exp})}$, is based on the first visible crack in the pure bending region. The predicted cracking moments, $M_{cr(\text{theo})}$, were calculated based on the modulus of rupture f_{cr}

$$M_{cr} = \frac{f_{cr} \cdot I_g}{y_t} N - mm; f_r = 0.7 \sqrt{f'_c} MPa$$

Where: I_g : gross moment of inertia, y_t : distance between NA and extreme tension fiber

The obtained ratio of the $M_{cr(\text{exp})}$ to the corresponding $M_{cr(\text{Theo})}$ is tabulated in Table 8

Conclusion

Load and Deflection behavior

- Load deflection curve of all the test beams specimens shows linear variation up to first crack level and behave in non-linear way with further increase in load.
- The first crack load are 11.77 KN, 32.24 KN, 17.65 KN, 19.62 KN, 28.44 KN, 30.39 KN for Case A, B, C, D, E and F respectively. Case F shows the highest first crack load among all the layered test beam specimens
- The ultimate load are 98.51 KN, 142.53 KN, 117.97 KN, 119.02KN, 128.25 KN and 134.25 KN for Case A, B, C, D, E and F respectively. Case F shows the highest ultimate load among all the layered test beam specimens

Energy Absorption Capacity

All layered test beam specimens shows increase in energy absorption capacity w.r.to M20 (Case A) by 53.10%, 81.40%, 123.60% and 137.40% for Case C, Case D, Case E and Case F respectively.

Toughness Index

All layered test beam specimens shows increase in toughness index w.r.to M20 (Case A) by 40.40%, 58.54%, 87.80% and 111% for Case C, Case D, Case E and Case F respectively.

Ductility Index

All layered test beam specimens shows increase in ductility index w.r.to M20 (Case A) by 39.15%, 49.70%, 57% and 65.80% for Case C, Case D, Case E and Case F respectively.

Cracking Moment

The cracking moment of all the layered beams shows increasing order w.r.to M20 (Case A), by 46%, 61.40%, 130.40% and 144.60% for Case C, Case D, Case E and Case F respectively. It can be concluded that Case F ($M_{60}/M_{20}/M_{60}$, 30% of M_{60} grade of concrete at upper layer/portion, 35% of

M_{20} grade of concrete at middle layer/portion and 35% of M_{60} grade of concrete at bottom layer/portion) shows better energy absorption capacity, toughness index, ductility index and cracking moment as compared to the other Cases.

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